Life cycle assessment for solid waste management in Lebanon: Economic implications of carbon credit



Waste Management & Research 2019, Vol. 37(1) Supplement 14-26 © The Author(s) 2018 Article reuse guidelines: sagepub.com/journals-permissions DOI: 10.1177/0734242X18815951 journals.sagepub.com/home/wmr (\$)SAGE



Abstract

Solid waste management has witnessed much progress in recent years with considerable efforts targeting the reduction of associated impacts and carbon emissions. Such efforts remain relatively limited in developing economies due to inefficient management practices. In this study, a life cycle assessment (LCA) approach is adopted to identify integrated systems with minimal impacts and reduced emissions in a developing context coupled with an economic valuation and sensitivity analysis to assess the effect of varying influencing parameters individually. The results showed that the highest impact arises from landfilling with minimal material recovery for recycling and composting, while incineration coupled with energy recovery contributed to the least equivalent emissions (-111% with respect to baseline scenario) at a varying cost of -70% to +93% depending on the selected technology and the value of carbon credit. Optimizing material recycling, composting and landfilling with energy recovery contributed to 98% savings in emissions (with respect to baseline scenario) and remained economically attractive irrespective of the carbon credit exchange rate of 0.5–50 US\$/MTCO₂E. The sensitivity analysis showed that an improvement in landfill gas collection efficiency (up to 60%) can contribute to major savings in emissions (58%). The application of the LCA-based approach supports the development of integrated viable plans while quantifying advantages and disadvantages towards decision-making and policy-planning.

Keywords

Integrated waste management, life cycle assessment, emissions estimation, economic analysis, carbon credit

Received 6th July 2018, accepted 12th October 2018 by Associate Editor David Ross.

Introduction

Population growth, development, and limited land resources around urban areas are curtailing waste management efforts in cities with inadequate planning policies (Arena et al., 2003). As such, solid waste is increasingly raising serious challenges and environmental concerns due to inefficient systems particularly in developing countries where landfilling remains the preferred route due primarily to economic factors or lack of technical expertise in other alternatives (e.g., biological and/or thermal treatment). The impacts of conventional landfilling have been long documented (El-Fadel et al., 1997). Its contribution to greenhouse gas emissions reaches $\sim 3\%$ worldwide and up to 15% in developing economies (Blanco et al., 2014). Thus, the proper selection of waste processing technologies through an integrated waste management system with minimal impacts and reduced emissions is imperative. In this context, the life cycle assessment (LCA) approach has been recognized as a valuable tool widely adopted as an internationally standardized method (International Organization for Standardization, 2006a, 2006b) that is effective in quantifying environmental impacts of management alternatives, thus contributing towards the decisionmaking process through the comparison of various systems.

Accordingly, several LCA-based accounting tools have been developed for estimating emissions from such systems (Gentil et al., 2010; Laurent et al., 2014a, 2014b). Recent efforts targeted LCA applications in the environmental assessment of waste management. Many of these efforts focused on developed economies (Di Maria and Sisani, 2017; Di Maria et al., 2016; Herva et al., 2014; Ripa et al., 2017; Thomsen et al., 2017; Tunesi et al., 2016) with limited applications on economies in transition or developing economies (Liu et al., 2017a, 2017b; Noya et al., 2018; Othman et al., 2013) where waste composition is different and management practices still concentrate on landfilling or open dumping (Laurent et al., 2014a, 2014b). In addition, most studies emphasized individual processes instead of integrated systems (Laurent et al., 2014a, 2014b; Tabata et al., 2010). Accordingly, this study aims to

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Figure 1. General location of test area.

Table 1. Municipal solid waste composition (data extractedfrom Laceco/Ramboll, 2012).

Waste category	(%)
Food	53.4
Glass	3.4
Metals	2
Nappies	3.6
Papers	15.6
Plastics	13.8
Textiles	2.8
Wood	0.8
Others	4.6
Total	100

fill a gap in a developing context particularly with respect to the effect of waste composition and integrated systems. For this purpose, an LCA approach is adopted at the system level to identify alternatives with minimal environmental impacts and reduced emissions. An economic valuation, a sensitivity analysis, and comparative assessment defined economically attractive scenarios taking into consideration related carbon credit.

Materials and methods

LCA analysis

The LCA was conducted in accordance with the ISO 14040 standards (International Organization for Standardization, 2006a, 2006b) and International Reference Life Cycle Data System (ILCD) Handbook (European Commission, 2010). Accordingly, four main steps were considered in the LCA study: goal and scope definition; inventory analysis; impact assessment; and interpretation.

Goal and scope. The LCA methodology was used to compare waste management alternatives and assess corresponding environmental

impacts. The test area (Beirut, Lebanon) encompasses 297 municipalities (Figure 1) with > 2M inhabitants generating 2,800-3,000 tonnes of municipal solid waste (MSW) daily with an average waste composition presented in Table 1. Waste is collected daily by a fleet of 332 collection vehicles that consume an average volume of diesel equivalent to 6.3 L/tonne of waste generated. The latter was calculated based on an overall diesel fuel consumption per year from various types of collection vehicles used in the test area. The data were used to estimate the average fuel consumed per tonne of waste collected. A comparison between international fuel consumption data and results from the test area shows that on average the resultant fuel consumption is comparable to the average reported value of 6 L/tonne of waste (Chen and Lin, 2008; Tanskanen and Kaila, 2001). When compared with other data reported in the literature from developed economies (Larsen et al., 2009), the consumption fell at the lower end of reported ranges of 6.3 and 10.1 L/tonne of waste from rural areas. However, adequate details on corresponding tested areas were not provided to allow a more accurate quantitative comparison, particularly that some studies suggest a lower range of 2.8–3.6 L/tonne of waste for high density urban areas (Nguyen and Wilson, 2010). In the local context, several factors may influence the higher fuel consumption, mainly traffic congestion that affects the number of traffic-related stops, location of transfer stations, as well as inefficient routes, and age of vehicles (Sonesson, 2000).

Functional unit (FU) and system boundaries. The FU was the management of 1 tonne of waste generated in the test area. The FU was also assumed as the reference flow on which the analysis was performed. Several scenarios were simulated to compare alternative management systems while considering the emissions to the environment, economic implications, and carbon credit. Figure 2 depicts the waste treatment processes and systems' boundaries (defined inside the frame boundaries) of the



Figure 2. Systems' boundaries for tested scenarios: S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S3, material recovery facility + maximum recycling and composting + landfilling; S4, maximum recycling and anaerobic digestion + landfilling; and S5, incinerate all waste + energy recovery.

tested scenarios. The systems' boundaries include emissions from waste management including indirect upstream emissions arising from inputs of materials and energy (electricity and fuel), direct operational emissions from systems' operation such as onsite operating equipment and waste degradation, and indirect downstream emissions related to energy generation, materials substitution, management of residues, and carbon storage.

The baseline scenario (S1) reflects a policy towards landfilling of all the waste with landfill gas (LFG) flaring because economic considerations render landfills as most attractive. Scenario S2 replaces flaring in S1 with energy recovery. However, land availability is continuously constraining landfilling particularly in urban areas. Hence, three other scenarios targeted the minimization of landfilling and optimization of recycling and biological treatment: composting (S3); anaerobic digestion (AD) –(S4); or incineration with energy recovery (S5).

Life cycle inventory (LCI). In a review of 220 waste-LCA studies, Laurent et al. (2014b) reported that around half of them favored the use of dedicated waste-LCA models instead of general LCA models. As such, in this study, the dedicated waste-LCA EASETECH software (Clavreul et al., 2014; Laurent et al., 2014b; Liu et al., 2017a, 2017b) was tailored to reflect the test area characteristics (waste composition, electricity mix, waste management, etc.) and applied to assess the environmental impacts of various waste management processes and estimate corresponding emissions. The data were collected from annual reports of facility operations, published sources, face-to-face interviews, site visits and field observations, and supplemented with reported literature. Table 2 synthesizes the input data of tested scenarios for assessing waste management processes.

The tested systems include the collection of mostly commingled waste that is transported to a material recovery facility with a recycling program, biological treatment (composting-AD), incineration, and landfilling (Table 2) with energy recovery when applicable. Input data for landfilling are summarized in Table 3 with several modules combined to represent this process: (1) construction and operation of the landfill; (2) gas generation using first order decay for a 100 years-time horizon and natural oxidation (in daily, intermediate, and final covers); (3) leachate generation (without treatment); and (4) stored substances in the landfill contribute to eco-toxicity and sequestrated carbon. The LCI data for individual waste treatment processes, extracted from the EASETECH database, are detailed in the Supplementary Material (Tables SM3-SM7). Waste collection was simulated for all scenarios based on an overall fuel consumption per year. Electricity requirements were derived using the Ecoinvent database (Ecoinvent, 2017) based on the country's national electricity mix, that rely primarily on oil-fired power plants (95.5%) and a small contribution from hydropower plants (4.5%) (MoE/UNDP/ GEF, 2015a).

Impact assessment. The ILCD (European Commission-JRC, 2011) impact assessment method was used in this study and is further described in Hauschild et al. (2013). The impact assessment was conducted for all scenarios using several indicators including climate change (global warming potential of 100 years-time horizon), photochemical oxidant formation, stratospheric ozone depletion, acidification, depletion of abiotic resources, and

Table 2.	Input data d	of tested	scenarios for	- assessing	waste ma	anagement	processes.

Identification number	Scenario	Description
51 52 53	Landfilling (100%) with flaring Landfilling (100%) with energy recovery MRF with recycling (15%) + composting (50%) + landfilling (35%) with flaring	 Landfilling of waste with LFG collection and flaring at 18% (MoE/UNDP/GEF, 2015b) Increase in the LFG collection efficiency up to 52% (DTU, 2017) with energy recovery facilities Commingled waste collected and transferred to two MRFs prior to treatment for material recovery (cardboard/paper (43.22%), metal (16.85%), glass (6.47%), plastic (33.46%) Laceco/Ramboll (2012)] and recycling or the removal of inert residues The 15% recovery rate is consistent with studies implementing successful recycling programs (Di Maria et al., 2013, 2015). Existing MRFs in the study area achieved a recycling recovery rate close to 10% by mechanical separation using bag openers, trommel screens, and magnetic separation with manual sorting (CDR-LACECO, 2014). With separation at source, it is expected that this rate can reach the 15% adopted in this study 81% of the recovered recyclables are sold for recycling industries the rest is sent for landfilling (CDR-LACECO, 2014) Simulated recycling processes include: shredding and reprocessing of mixed paper and cardboard material; shredding and reprocessing of steel scrap. Note that inventory data of avoided emissions form recycling processes were adopted from the EASETECH database (DTU, 2017) Food waste is treated using open windrow composting at 300 tonnes/day with air supplied by mechanical turning using wheeled loader The resulting compost has a C/N ratio of 16.5, pH of 7.3, average density of 470 kg/m3, average nitrogen content of 1.44%, average organic content of 52.6%, and moisture content of 48% by wet weight (CDR-LACECO, 2014). However, the compost has not been well-accepted with farmers mostly because it contains a small fraction of glass due to no separation of waste at source Non-sold compost used as a cover material at the landfill The consumption of electricity and fuel during operation are 0.02 kWh/tonne of waste composted and 3.28 liters/tonne of
S4	Sorting at source + recycling (15%) + AD (50%) with energy recovery + landfilling (35%) with flaring	 (Boldrin et al., 2009) The remaining waste stream is landfilled with LFG flaring Waste management involves sorting-separation at source prior to the AD treatment. The source separation efficiency by individual waste component is presented in the supplementary material (see Supplementary Material Table S2) The average electricity production is around 244 kWh/tonne (based on a range of 184–299 kWh/tonne) with engine conversion efficiency of 36% (Møller et al., 2009) Digestate used in land application and as a substitute for fertilizer production Methane leakage rate from AD assumed at 10% (DTU, 2017) Energy consumption at 49 kWh of electricity and 0.9 L of diesel/tonne of organic waste (DTU, 2017) The LCI data of AD are adopted from the EASETECH database (DTU, 2017) based on an average biogas plant in Europe using a one stage wet
55	Incineration (100%) with energy recovery	 thermophilic anaerobic digestion process for the treatment of the organic fraction of municipal solid waste (see Supplementary Material Table SM5) All MSW is collected for incineration coupled with energy recovery LCI data of incineration are adopted from a typical incineration plant in Denmark, which was selected from the EASETECH database (DTU, 2017) and adjusted using the waste composition and specific data of the test area (see Supplementary Material Table SM6) Given the higher moisture of the MSW in the test area, an 18% net electricity output efficiency (after subtracting the operational energy consumed within the facility) was adopted (Chen and Christensen, 2010; Di Maria and Pavesi, 2006; Di Maria et al., 2018; Liu et al., 2017a, 2017b; Münster and Lund, 2010)

Table 2. (Continued)

ldentification number	Scenario	Description
		 Average calorific value of the waste in the test area is 6.9 MJ/Kg [Laceco/ Ramboll, 2012], which is at the edge of the upper range of the LHV that is 5-6 MJ/ kg required to sustain the burning process (Chen and Christensen, 2010; Di Maria et al., 2018) and avoided auxiliary equipment (Zhao et al., 2012) Diesel fuel consumed for the operation of the facility was considered at 1 liter/tonne of waste incinerated (Astrup et al., 2009) Requires electricity input of 70 kWh/tonne of waste and generates 20% ash (Fernandez-Nava et al., 2014; Yay, 2015) Fly ash exported and used as backfilling in salt mines and bottom ash delivered to inert landfilling without energy recovery

Notes: L, landfilling; I, incineration: R, recycling; C, composting; MRF, material recovery facility; AD, anaerobic digestion; MSW, municipal solid waste; LFG, landfill gas; LHV, lower heating value; and LCI, life cycle inventory.

Table 3. Data on consumption, expressed per tonne of waste for landfilling (DTU, 2017; Manfredi et al., 2009).

Consumption	Value
Electricity (kWh)	8
Diesel fuel consumption (L)	2
Steel sheets (tonne)	0.00014
Aluminum (tonne)	5.8 × 10 ⁻⁸
Polyvinylchloride resin (tonne)	10 ⁻⁵
Polyvinylchloride fibers (tonne)	4 × 10 ⁻⁸
Polyethylene high density granulate (tonne)	0.00023
Gravel (tonne)	0.18
Clay (tonne)	0.082
Copper (tonne)	9.87 × 10 ⁻⁹

freshwater and marine eutrophication. The model results are presented in the form of characterized and normalized potential impacts. The latter is expressed as person equivalent, which is the contribution to an indicator of an average person in a given reference year as outlined in Table 4.

Economic analysis

The cost of management alternatives was estimated using an average cost for the total amount of waste managed under each scenario (Table 5). The wider range in Table 5 is considered in the sensitivity analysis to define breakeven points that could assist in defining zones of enhanced economic viability. Inflation was not included, and values were considered at a constant year zero. The offset of emissions was quantified based on the carbon market. The latter ranged from 0.5–50 US\$ per metric tonne of carbon dioxide equivalent (MTCO₂E) in 2016, with an average price of 3 US\$/MTCO₂E, which is the lowest reported market value from voluntary actors since 2006 (Ecosystem Marketplace, 2017). The average value was used to assess associated benefits and allows for the estimation of minimal savings when the carbon footprint is reduced through regulated and voluntary global markets for trading or offsetting of carbon credits. A wider range

is considered in the sensitivity analysis to define breakeven points that could assist in decision-making and policy-planning.

Sensitivity analysis

A one-factor-at-a-time sensitivity analysis was conducted to assess key parameters by varying the main assumptions whereby each parameter was varied one at a time to assess its impact on emissions. These parameters included the fraction of the LFG collected, food waste fraction, land application of compost, and net energy recovery efficiency of waste incineration. The cost range of carbon credit and several waste management processes (AD, incineration and landfilling with energy recovery) were also considered one at a time to assess their impacts on net cost variations and define breakeven points for decision-making and policy-planning. Note that only processes related to alternative technologies were tested for cost variation, because for the baseline scenario (landfilling, sorting/recycling, and composting) the costs are already fixed.

Results and discussion

LCA analysis

The results of the LCA characterization analysis per functional unit (1 tonne of MSW managed) for each indicator of the tested scenarios are depicted in Figure 3 taking the baseline scenario (S1) as the normative reference, whereby all other scenarios are indexed to the impact of S1 per 1 tonne of MSW (S1 is 100%). Figure 4 depicts the contribution of each scenario disaggregated by waste management processes to the impact categories. The results show that landfilling scenarios contribute the most to all impact categories (Figure 3). For instance, the baseline scenario S1 that consists of landfilling all waste with flaring of LFG collected (18%) is associated with the highest climate change impact (global warming potential GWP₁₀₀) in comparison to other scenarios due to uncaptured methane emissions from landfilling (Figure 4a). Note that developing economies are generally

Impact category	Characterization unit	Global normalization reference ^a (2010 or 2013)
Climate change, global warming potential GWP _{100b}	Kg CO ₂ -equivalents	8100
Photochemical oxidant formation	Kg NMVOC	56.7
Stratospheric ozone depletion	Kg CFC-11-equivalents	0.0414
Acidification	Kg SO ₂ -equivalents	74
Freshwater eutrophication	Kg P-equivalents	0.62
Marine eutrophication	Kg N-equivalents	9.38
Depletion of abiotic resources	MJ	6.24 × 10 ⁴

Table 4. Normalization references for the selected environmental impact categories (DTU, 2017; Laurent et al., 2013).

Notes: ^acharacterization unit/person/year: person equivalent = characterized impact category (characterization unit)/normalized reference (characterization unit/person/year); and ^b note that the global warming potential GWP₁₀₀ that was selected in this study follows the IPCC 2013 reference (Myhre et al., 2013), including climate–carbon feedbacks.

Table 5. Average cost of municipal solid waste management (US\$/tonne of waste).

	Collection and transport	Sorting	Composting	Anaerobic digestion with energy recovery	Landfilling	Landfilling with energy recovery	Incineration with energy recovery
MoE/UNDP/ECODIT (2011); CDR (2010)	33	23	25	_	46	-	-
Maalouf and El-Fadel (2017)	20-250	26-28	5-90	20-150	10-100	13–67	-
Assamoi and Lawryshyn (2012)	_	-	-	-	18	-	38
Dijkgraaf and Vollebergh (2004)	_	-	-	-	45	-	97
European Commission (2002)	_	-	-	80	62	58	88
Jamasb and Nepal (2010)	_	26	-	-	15	13	70
Rabl et al. (2008)	-	-	-	-	45	40	92
Tsilemou and Panagiotakopoulos (2006)	_	-	17–73	22–67	12-50	-	117
World Bank (2012)	20-250	-	5-90	20-150	10-100	-	120
WRAP (2016)	-	28	27	44	21	-	94
Range (US\$/tonne)	20-250	23–28	5-90	20-150	10-100	13–67	38-120
Adopted average (US\$/tonne)	33ª	23ª	25ª	85 ^b	46 ^a	57°	90 ^d

Notes: ^acurrent-costs in the test area applied for the baseline scenario (S1). Costs exclude leachate treatment; ^banaerobic digestion includes energy recovery but excludes cost of residue sale or disposal; ^caverage including an additional ~17 US\$/tonne of waste for onsite leachate and gas management (Damgaard et al., 2011; European Commission, 2002); and ^dincludes energy recovery but excludes disposal cost of bottom and fly ash.

characterized by poorly operated landfills with inefficient LFG collection systems at efficiencies ranging between 28% and 40% (Banar et al., 2009) compared with 60% to-98% reported in developed economies (EPA/ICF, 2016). In this case, the low collection efficiency can be attributed to the high fraction of the food waste component associated with rapid decomposition leading to unstable LFG generation; the high moisture content of the waste resulting in the generation of large quantities of leachate that reduce the collection efficiency; and inefficient gas recovery systems (Liu et al., 2017 a, 2017b; Zhan et al., 2015). The sensitivity analysis showed that a 10% increase in the food waste fraction, led to an equivalent increase of 8.6% in the climate change impact indicator (Table 6). This can be attributed to emissions through the landfill surface during the early stage of waste disposal (1-2 years). Similarly, an increase in the LFG collection efficiency up to 60%, contributed to a 58% decrease in the climate change impact indicator (Table 6). Major savings

in the climate change impact were achieved under scenario S4 considering incineration with energy recovery (Figure 4a). In this context, results from sensitivity analysis showed that a 10% increase in the electricity efficiency from incineration could save 53% of the climate change impact indicators (Table 6).

All scenarios except S3 and S4 exhibited a similar trend for the depletion of abiotic resources due to avoided raw material usage through recycling. Moreover, waste collection has a significant impact in this category due to the use of fossil fuels (Figure 4e). The waste composition exhibited different impacts on emissions from various treatment processes. For instance, the high fraction of biodegradable food waste was advantageous to the AD process whereby more biogas generation for energy recovery would result in greater savings in emissions. However, environmental benefits from these scenarios are affected by several factors such as gas leakage under AD and land application of compost or digestive residues. In the case of the test area, food waste is not separated at

=2



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reference, whereby all other scenarios are indexed to the impact of S1 per 1 tonne of MSW (S1 is 100%): S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S3, maximum recycling and composting + landfilling; S4, maximum recycling and anaerobic digestion + landfilling; and S5, incinerate all waste + energy recovery.

the source contributing to a lower efficiency of separation which translates into less emissions savings. The low-quality compost in the test area is invariably not accepted by farmers and hence used as intermediate covers in landfilling, thereby contributing to greater emissions. Accordingly, the separation of waste at source will contribute to about 11% savings in acidification and 7% in photochemical oxidant formation (Table 6). This can be attributed to the production of better-quality compost that can be used on land, resulting in savings from the substitution of fertilizer production and carbon storage. Further savings can also be attributed to avoided energy consumption during pretreatment.

Stratospheric ozone depletion is caused by emitting "methane bromotrifluoro-Halon 1301," which is a consequence of crude oil production, petroleum, and natural gas (Yay, 2015). The best alternative against ozone depletion is scenario S5 that considers incineration with energy recovery substituting electricity production from oil-fired power plants in the case of the test area (Figure 4c). However, the benefits of waste incineration can be compromised by the high organic fraction and moisture content that decrease the net energy recovery in comparison to developed economies at 30% to 31% (Gohlke and Martin, 2007; Murer et al., 2011).

Landfilling scenarios contribute mostly to the photochemical oxidant formation due to methane emissions, with savings achieved under scenarios S3 and S4 considering the minimization of landfilling in comparison to the baseline scenario S1 (Figure 3). Waste collection also contributes to the effect of photochemical oxidation due to sulfur dioxide (SO₂) emissions (Figure 4b). The acidification potential is measured by its capacity to form H⁺ ions relative to SO₂ (Banar et al., 2009; Yay, 2015). Energy recovery is the best alternative to reduce this impact due to savings in NO_x emissions from equivalent electricity generation. Accordingly, incineration coupled with energy recovery (scenario S5) achieved the most savings from this category followed by upgrading the LFG collection system from flaring to energy recovery (scenario S2) (Figure 3). Alternative scenario S4 that considers AD also reduced the impact of acidification due to the use of biogas for energy recovery and digestate in farming as a substitute for fertilizer production (Figure 4d). Similarly, this scenario achieved significant savings in freshwater eutrophication due to avoided fertilizer production and energy recovery (Figure 4f). However, S4 might affect marine eutrophication due to nitrate run-off from the application of digestate on land (Hansen et al., 2006; Yay, 2015).

In summary, the comparison of scenarios (Figure 5) using the normalized potential impacts showed that the integrated MSW management system is contributing most to the climate change indicator. While, the highest impact arises from landfilling all waste (scenario S1), mainly due to uncaptured methane emissions, the greatest benefits can be derived from incinerating all the waste (scenario S5) due to energy recovery. Similarly, maximizing recycling and composting or AD in scenarios S3 and S4 contributed to significant savings in all impact categories.

Economic analysis

Reducing emissions from alternative scenarios can be subject to economic constraints depending on the technology adopted

2000

1000

-1000

-2000

-3000

0



Figure 4. Contribution of each scenario to the impact categories: S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S3, maximum recycling and composting + landfilling; S4, maximum recycling and anaerobic digestion + landfilling; and S5, incinerate all waste + energy recovery.

and whether reductions are considered in the economic valuation (Table 7). In the context of the existing waste management system, maximizing waste recycling and composting with minimal landfilling decreases the management cost most (-21%) with carbon credit). Optimizing emissions reduction through incineration and energy recovery (S5) reduces emissions most at the expense of an overall increase in cost (+52% with carbon credit) (Table 7). The breakeven analysis defines when the

Parameter		Climate changeª	Acidification ^b	Photochemical oxidant formation ^c	Comments
Food waste fraction	Initial value (53.4 %) Increase 10% % change	859.5 (S1) 932.9 +8.6%	0.27 (S1) 0.28 +5.5%	0.63 (S1) 0.67 +6.3%	The change in the food waste fraction had a great impact on emissions (Liu et al., 2017a) % change considering 53.4 to 58.7
Landfill gas collected	Initial value (18 %) New value (60%) % change	859.5 (S1) 58.2 <i>-58.3%</i>	0.27 (S1) 0.27 -1%	0.63 (S1) 0.47 -24.4%	Collection efficiency of (60%) for a typical operating landfill with wet waste (EPA/ICF, 2016). % change considering 18 to 60
Land application of compost	Without With % change	19.9 (S3) 19.8 -0.5%	0.12 (S3) 0.10 <i>-11.1%</i>	-0.14 (S3) -0.15 -7.1%	Avoided emissions from the application of compost as a fertilizer are adapted from (Boldrin et al., 2009; DTU, 2017) assuming the waste is co-composted with a nutrient material % change from not considering land application of compost to considering it
Net energy recovery efficiency of waste incineration	Initial value (18 %) Increase 10% <i>% change</i>	–90.5 (S5) –138.5 <i>–53%</i>	–5.71 (S5) –6.36 –11.4%	-0.81(S5) -1 <i>-23.2%</i>	Given the higher moisture of municipal solid waste characteristic of the test area, the net electricity output efficiency was set at 18% (Chen and Christensen, 2010; Di Maria et al., 2018; Liu et al., 2017a, 2017b). % change considering 18–19.8

Table 6. Sensitivity to key input parameters.

Notes: S1, baseline scenario: landfilling with flaring; S3, maximum recycling and composting + landfilling; and S5, incinerate + energy recovery. The percentage change is calculated with respect to the total initial value of the different impact categories (expressed depending in the characterization unit): ^aimpact on climate change expressed in Kg C0₂E/tonne of waste; ^bacidification potential expressed in Kg S0₂E/tonne of waste; and ^cphotochemical oxidant formation expressed in Kg NMVOC/tonne of waste.



Figure 5. Normalized potential non-toxic impacts from the treatment of 1 tonne of municipal solid waste: S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S3, maximum, recycling and composting + landfilling; S4, maximum recycling and anaerobic digestion + landfilling; and S5, incinerate all waste + energy recovery.

carbon credit could enhance the economic viability of adopting a favorable policy towards a technology change. Holding the same value for all parameters, Figure 6 depicts the breakeven points for all scenarios taking into consideration only the reported cost range of carbon credit (0.5-50 US\$/MTCO₂E). While scenarios S2 and S4 become economically viable at a carbon credit cost of 21 US\$/MTCO₂E, scenario S3 stipulating maximum recycling and composting with landfilling remains profitable under the entire range of carbon credit. On the other hand, incineration with energy recovery under scenario S5 requires the highest capital investment and cannot achieve overall economic attractiveness except under the highest car-

Table 7. Economic implications of scenario analys	IS.
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Scenario	Description	Avoided emissions (%)	Cost variation (%)
S1	Collection + landfilling with gas flaring	0 (baseline)	0 (baseline)
S2	Collection + landfilling + with landfill gas energy recovery	-63	12
S3	Collection + maximum recycling and composting + landfilling with gas flaring	-98	-21
S4	Collection + maximum recycling and anaerobic digestion + landfilling with gas flaring	-101	17
S5	Collection + incineration + energy recovery	-111	52

Notes: avoided emissions (climate change impact indicator) is calculated with respect to existing total emissions of baseline scenario (S1) whereby *Avoided emissions* % = [(*Old – New*)/*Old*] where Old = total emissions of baseline scenario (S1) and New = total net emissions of alternative scenario S₁ where i = 2–5; cost variation is calculated with respect to existing costs of baseline scenario (S1) whereby *Cost variation* % = [(*Old – New*)/*Old*] × 100 where Old = total cost of baseline scenario (S1) and New = total cost of alternative scenario S₁ where i = 2–5; and note that the cost variation includes environmental externalities in the form of carbon credit that is based on 3 US\$/MTCO₂E (Ecosystem Market-place, 2017).



Figure 6. Breakeven point analysis for carbon credit with respect to baseline scenario S1: S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S3, maximum recycling and composting + landfilling; S4, maximum recycling and anaerobic digestion + landfilling; and S5, incinerate all waste + energy recovery.

bon credit cost of \sim 50 US\$/MTCO₂E, albeit showing the greatest potential for emissions reduction.

The sensitivity analysis for all scenarios showed a significant change in the economic impact ranging from -76% to +93% at a cost range of carbon credit of 0.5 and 50 US\$/MTCO₂E (Figure 7). Incineration with energy recovery contributed most to the variation in cost that ranged between -70% and 93% with respect to the baseline scenario S1 (Figure 7). Energy recovery of LFG collected instead of flaring (S1) can contribute to significant savings in cost that reached 76% with respect to S1 at a higher carbon credit exchange rate (Figure 7). Similar to incineration, the cost of AD with energy recovery varies widely from -76% to 61% with respect to the baseline scenario S1 (Figure 7).

It is worth mentioning that other externalities (e.g., real estate depreciation, air and groundwater pollution with potential health impacts) may affect the economic valuation of various scenarios. Another limitation is related to time factor considerations that affect both costs and emissions (e.g., time required for the construction of different waste facilities). Moreover, current and future offsets of electricity were assumed similar.

Conclusion

The LCA was applied in evaluating waste management alternatives towards defining optimal integrated systems. The highest environmental impacts were associated with scenarios that include landfilling with minimal material and energy recovery. Environmental benefits can be achieved under scenarios that maximize recycling and composting whereby cost savings in emissions reached up to 98%. Incineration with energy recovery reduced equivalent emissions most at a varying cost of -70% to +93% depending on the selected technology and the value



Figure 7. Sensitivity to the cost of waste management processes and carbon credit (comparison with baseline scenario S1): SLL, process and carbon credit costs set at their lowest values; SLH, process cost set at its lowest value and carbon credit at its highest; SHL, process cost set at its highest value and carbon credit at its lowest; SHH, process cost set and carbon credit set at their highest values; S1, baseline scenario: landfilling all waste with flaring; S2, upgrade landfill gas capture system in S1 + energy recovery; S4, maximum recycling and anaerobic digestion + landfilling; S5, incinerate all waste + energy recovery.

of carbon credit. Despite the decrease in emissions, increased operational and investment costs favor alternatives that consider maximizing recycling and composting with residual landfilling when land is available. The sensitivity analysis suggested that greater savings in emissions can be achieved with improved landfill gas collection efficiency, application of produced compost, and energy recovery during incineration. Finally, the breakeven analysis showed that maximizing material recovery and landfilling remains profitable under the entire range of carbon credit (0.5-50 US\$/MTCO₂E). While the results provide guide-lines for policy-planning and decision-makers on the economic viability of investment in carbon credit, potential changes in costs due to the dynamics of economy of scale and other externalities should be considered in the economic analysis.

Acknowledgements

Special thanks are extended to Dar Al-Handasah (Shair & Partners) for its support to the graduate programs in Engineering at the American University of Beirut.

Declaration of conflicting interests

The authors declared no potential conflicts of interest with respect to the research, authorship, and/or publication of this article.

Funding

The authors disclosed receipt of the following financial support for the research, authorship, and/or publication of this article: This study is supported by joint funding from the Lebanese National Council for Scientific Research (LNCSR) and the American University of Beirut (AUB). Access to the EASETECH software was provided by the Department of Environmental Engineering at the Technical University of Denmark.

Supplemental material

Supplemental material for this article is available online.

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